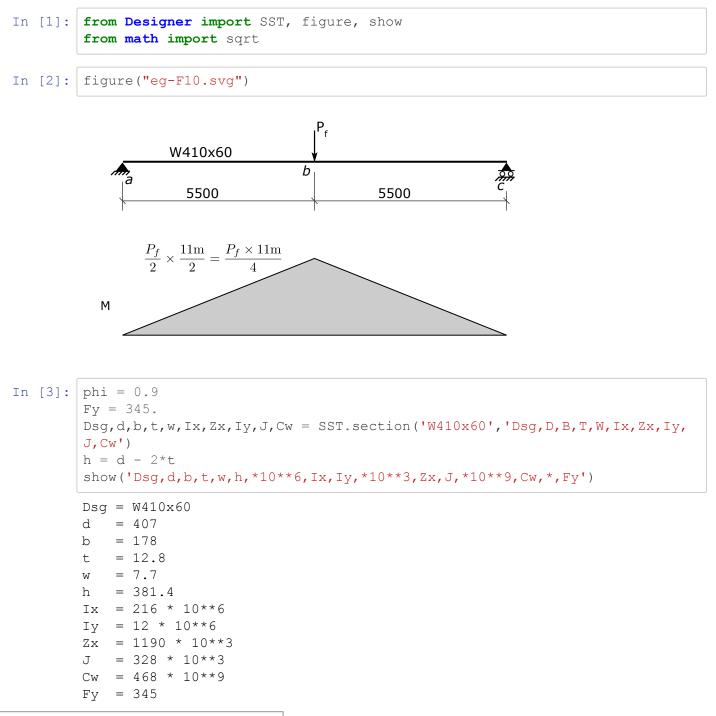
Example F10: Effect of lateral bracing.

For the following beam, compute the maximum factored load, P_{f} for the following three cases.

- Case a): compression flange fully braced laterally.
- Case b): compression flange braced only at the supports.
- Case c): compression flange braced at the supports and at the point of application of the load.

Use ASTM A992 steel.



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Check Local Buckling

```
In [4]: show('bel/t = b/(2*t), 170/sqrt(Fy)') # check flange against class 2 lim
its
bel/t = 6.953
170/sqrt(Fy) = 9.152
In [5]: show('h/w, 1700/sqrt(Fy)') # check web against class 2 limits
h/w = 49.53
1700/sqrt(Fy) = 91.52
```

Therefore section is class 2 (or perhaps class 1 - that doesn't matter)

Case a) fully braced

From § 13.5: $M_r = \phi M_p = \phi F_v Z_x$

In [6]: Mr = phi*Fy*Zx * 1E-6 # * 1E-6 converts from N-mm to kN-m
Pf = Mr * 4. / 11.
show('Mr,Pf')
Mr = 369.5
Pf = 134.4

For case a), maximum $P_f = 134$ kN.

Case b) lateral bracing at supports only

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The last paragraph of § 13.6 a) says the following:

_For unbraced beam segments loaded above the shear centre between brace points, where the method of load delivery to the member provides neither lateral nor rotational restraint to the member, the associated destabilizing effect shall be taken into account using a rational method. For loads applied at the level of the top flange, in lieu of a more accurate analysis, M_u may be determined using $\omega_2 = 1.0$ and using an effective length, for pin-ended beams, of 1.2L and for all other cases, 1.4L._

It seems reasonable that the above should apply to this case, so use an unbraced length of compression flange equal to 1.2 times the distance between supports.

S16-16 § 13.6 a) ii) gives the following for calculating M_{μ} :

$$M_{u} = \frac{\omega_{2}\pi}{L} \sqrt{EI_{y}GJ + \left(\frac{\pi E}{L}\right)^{2}I_{y}C_{w}}$$

Often, we re-write that to make it a little simpler to apply manually:

$$A = EI_y GJ$$
$$B = \left(\frac{\pi E}{L}\right)^2 I_y C_w$$
$$M_u = \frac{\omega_2 \pi}{L} \sqrt{A + B}$$

In [7]: pi = 3.14159 E = 200000. G = 77000.

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```
In [8]: omega2 = 1.0
        L = 1.2 \times 11000
         A = E * I y * G * J
         B = Iy*Cw* (pi*E/L) **2
         Mu = (omega2*pi/L)*sqrt(A+B) * 1E-6 # for result in kN-m
         Mp = Fy \star Zx \star 1E-6
         show('omega2,L,A,B,Mu,Mp,0.67*Mp')
         omega2 = 1
                = 13200
         L
         А
                = 6.061e+22
         В
                = 1.272e+22
        Mu
                = 64.45
        Mр
               = 410.6
        0.67 * Mp = 275.1
```

As $M_u \le 0.67 M_p$, $M_r = \phi M_u$:

In [9]: Mr = phi*Mu
Pf = Mr * 4. / 11.
show('Mr, Pf')
Mr = 58.01
Pf = 21.09

For case b), maximum $P_f = 21.1$ kN.

Case c) Lateral bracing at ends and at centre

From Figure 2-17 in the commentary, $\omega_2 = 1.75$.

Or, the long way from § 13.6 a) ii):

 $\kappa = 0$

(because in the beam segments between the brace points, *ab* and *bc*, the smallest end moment is 0, and 0/anything is zero, as long as *anything* \neq 0).

And then:

 $\omega_2 = 1.75 + 1.05\kappa + 0.3\kappa^2 = 1.75$

```
In [10]: omega2 = 1.75
         L = 5500.
         A = E * I y * G * J
         B = Iy*Cw* (pi*E/L) **2
         Mu = (omega2*pi/L)*sqrt(A+B) * 1E-6 # for result in kN-m
         Mp = Fy \star Zx \star 1E-6
         show('omega2,L,A,B,Mu,Mp,0.67*Mp')
         omega2 = 1.75
                 = 5500
         L
         А
                = 6.061e+22
                = 7.329e+22
         В
                = 365.8
         Mu
         Мр
                = 410.6
         0.67 * Mp = 275.1
```

In this case, $M_u > 0.67 M_p$ and thus M_r is given by § 13.6 a) i):

```
In [11]: Mr = min( 1.15*phi*Mp*(1 - 0.28*Mp/Mu), phi*Mp )
Pf = Mr * 4. / 11.
show('Mr,Pf')
Mr = 291.4
Pf = 106
```

For case c) maximum $P_f = 106$ kN.

Summary

| Case | P _f max. |
|------------------------------|---------------------|
| a) fully braced | 134 kN |
| b) braced at ends only | 21.1 kN |
| c) braced at ends and center | 106 kN |
| | |

In []: